

# IIP Update: A Packaged Coherent Doppler Wind Lidar Transceiver

"Doppler Aerosol WiNd lidar (DAWN)"

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to

Working Group on Space-Based Lidar Winds Welches, OR 27 June 2006





## IIP Key Personnel

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Also many thanks to Brian Killough, Keith Murray, Garnett Hutchinson, and Ken Anderson



## **IIP Motivation**

	Mission	Measurement Technique		Technology	
Primary	Science: Weather, Climate	Earth Vertical <b>Wind</b> Profiles	Scanning Doppler Lidar	Pulsed, 2-Micron, Ho Laser	
Secondary	Science: Climate	Earth Vertical <b>CO</b> <sub>2</sub> Concentration Profiles	Scanning DIAL Lidar	Pulsed, 2-Micron, Ho Laser	
	Science & Exploration: Atmos. Char., EDL	Mars Vertical <b>Density</b> Profiles	DIAL Lidar (CO <sub>2</sub> )	Pulsed, 2-Micron, Ho Laser	
	Science & Exploration: Atmos. Char., EDL	Mars Vertical <b>Wind</b> Profiles	Scanning Doppler Lidar	Pulsed, 2-Micron, Ho Laser	
	Science: Climate	Earth Vertical <b>Aerosol</b> Concentration Profiles	Backscatter Lidar	Pulsed, 2-Micron, Ho Laser	
	Science & Exploration: Atmos. Char., EDL	Mars Vertical <b>Dust</b> Profiles	Backscatter Lidar	Pulsed, 2-Micron, Ho Laser	



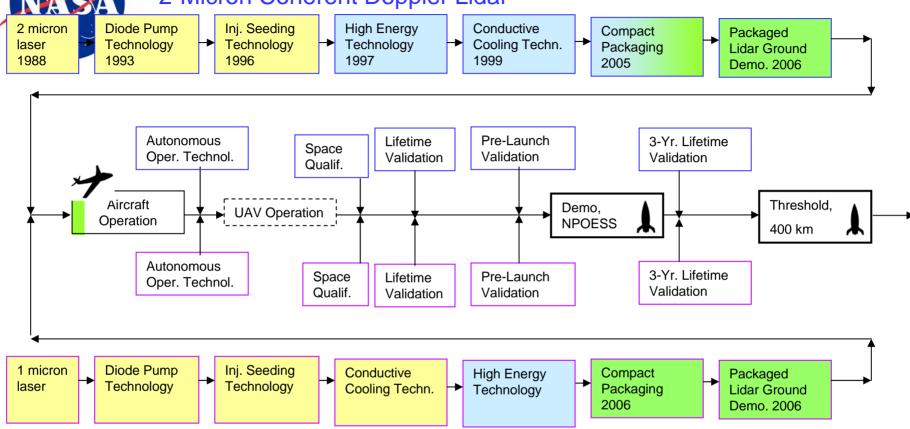
### **IIP Abstract**

The state-of-the-art 2-micron coherent Doppler wind lidar breadboard at NASA/LaRC will be engineered and compactly packaged consistent with future aircraft flights. The packaged transceiver will be integrated into a coherent Doppler wind lidar system test bed at LaRC. Atmospheric wind measurements will be made to validate the packaged technology.

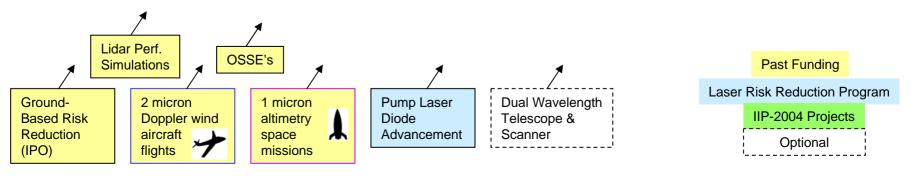
This will greatly advance the coherent part of the hybrid Doppler wind lidar solution to the need for global tropospheric wind measurements.

## IIP and the Global Tropospheric Wind Profiles Roadmap





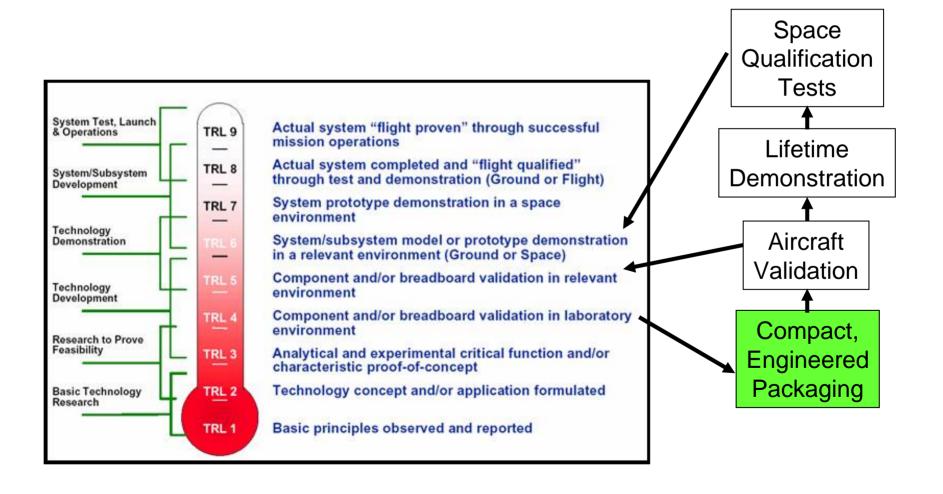
### 0.355-Micron Direct Doppler Lidar





### IIP TRL Advancement

" $4 \rightarrow 5$ "





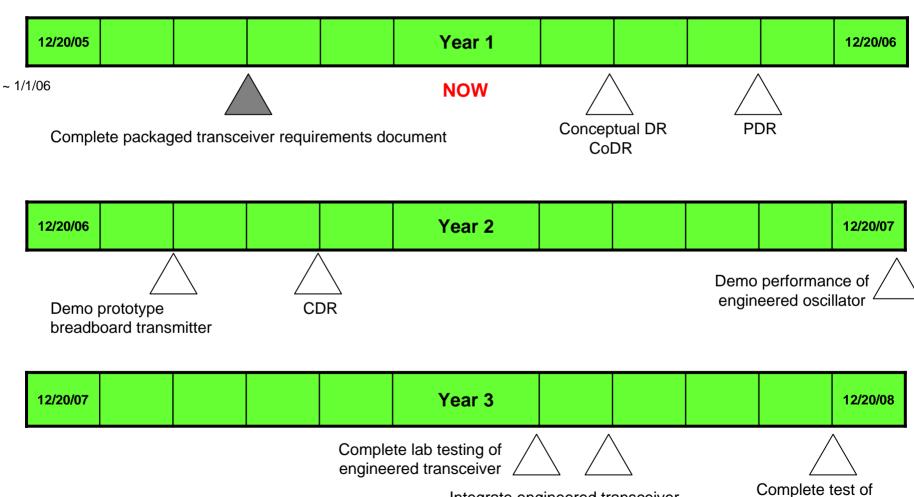
# IIP and the LaRC Development of Pulsed, 2-Micron Laser Technology For Space

Category	Sub-Category/Date	6/02	9/02	2/03	4/03	11/03	2/05	12/05	LRRP	IIP	SPACE DEMO
Demonstrated (Side-Pumped,	Pulse Energy (J) (in double pulse)	0.135	0.355 / <u>0.6</u>	0.095	0.626/ <u>1.05</u>	0.1/ 0.073	1/ <u>1.5</u>	1.2		0.25	0.25
LuLiF)	Pulse Rate (Hz)	2	2	10	2	2/10	2	2		10	5-10
	Efficiency (%) (O-O)	3.65	3.66	2.57	4.10	2.78	5/ <u>6.2</u>	6.5			
Laser	Oscillator	✓	✓	✓	✓	✓	✓	✓		✓	✓
Component	Preamplifier						✓				
	Amplifiers		1 x 2- pass		2 x 2- pass		2 x 2- pass	2 x 2- pass	<b>~</b>	1 x 2- pass	1 x 2-pass
Laser Mode	Q-Switched	✓	✓	✓	✓	✓	✓	✓		✓	✓
	Double Q-Switched		✓		✓	✓	✓				
	Injection Seeded=SLM			<b>✓</b>						✓	<b>✓</b>
Cooling	All liquid				amp						
	Partially conductive	✓	✓	✓	osc		✓	✓		✓	
	All cond w/o heat pipe										
	All cond w/ heat pipe					✓			✓		✓
Pump Diodes	C Package				amp						
	A package	✓	✓	✓	osc	✓	✓	✓	✓		
	AA package									✓	
	G package										✓
Packaging	Laboratory Table	✓	✓	laser	✓	laser	✓	✓			
	Compact, Engineered			head		head			head	✓	✓

7



### IIP- Milestones & Schedule



Integrate engineered transceiver

Into testbed

engineered transceiver

In lidar testbed



# IIP Packaged Transceiver Requirements

Category	Requirement	Goal (if different) and/or Space Requirement	Reason
Laser Architecture	Master Oscillator Power Amplifier (MOPA)		High energy, beam quality, optical damage
Laser Material	Ho:Tm:LuLiF		High energy, high efficiency, atmospheric transmission
Nominal Wavelength	2.053472 microns		Atmospheric transmission
Pulse Energy	150 mJ	250 (space)	Computer modeling of measurement performance
Pulse Repetition Frequency	10 Hz	10-20 (space)	Shot accumulation, optimum laser diode array lifetime
Pulse Beam Quality	< 1.4 x diffraction limit		Heterodyne detection efficiency influence
Pulse Spectrum	Single Frequency	Few MHz (space)	Frequency estimation process
Injection seeding success	95%	99%	Shot accumulation
Laser Heat Removal	Partial Conductively Cooled	FCC (space)	No liquid lines in space
Packaging	Compact, engineered	Aircraft ready Space qual. (space)	As ready as possible for aircraft follow on



## Oscillator features

- Injection seeded
- Cavity length
- Output coupler Reflectivity
- Diode pump lasers: conductive cooled
- crystal doped material length
- undoped LuLF length
- Laser crystal cooling :
- Tube size:
- Laser rod ends
- Laser rod cylinder

>3m Ring

~70%

36 bars 100W/b

**21mm** 

15 mm

H<sub>2</sub>O, Methanol

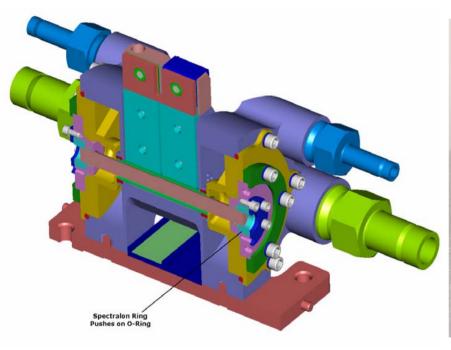
6mm OD 5mm ID AR coated for 792nm

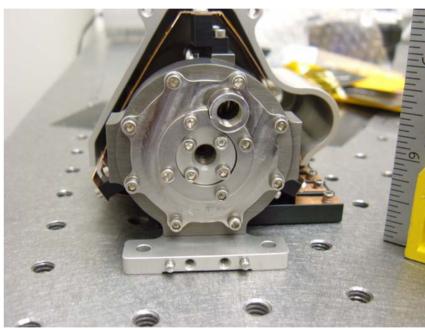
wedged 0.5° along c-axis AR coated for 2.053µm

AR coated for 792nm



## **Oscillator Head**







# Oscillator cavity length

- Long cavity length is needed to obtain narrow linewidth
  - Pulse length is one of the critical parameters of a coherent Lidar.
  - A short pulse compromises frequency resolution while a long pulse compromises range resolution.
  - To meet the pulse length requirement, the oscillator length was changed from 2m to 3m. It prolongs the pulse width to near 200ns
  - The resonator has six mirrors and 8 bounces.



# **Amplifier features**

- Pump energy
- Diode laser
- Laser crystal
- Doped Crystal length
- Ends diffusion bonded crystals
- Laser crystal cooling
- Flow tube size
- Rod end surfaces
- Laser cylinder
- Path configuration

7.2Joules12x6 bar arrays with 100watts/bar

conductive cooled 'AA' Pkg

Ho:Tm:LuLF 0.5% Ho 6%Tm

41mm

15 mm undoped LuLF

H<sub>2</sub>O

6mm OD 5mm ID AR coated 792nm

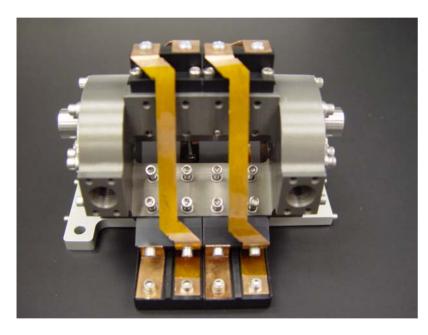
AR coated for 2.053μm

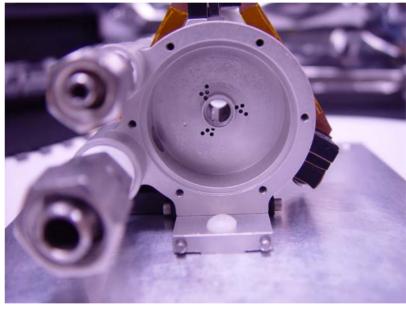
AR coated for 792nm

double pass



# **Amplifier Module**

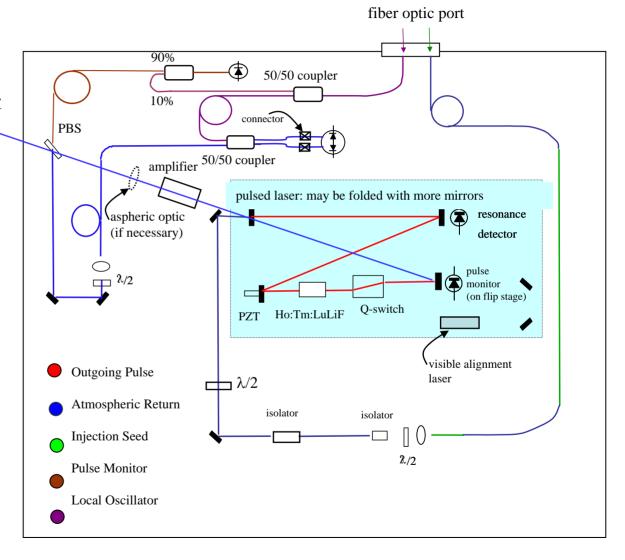






## Proposed Transceiver "Box"

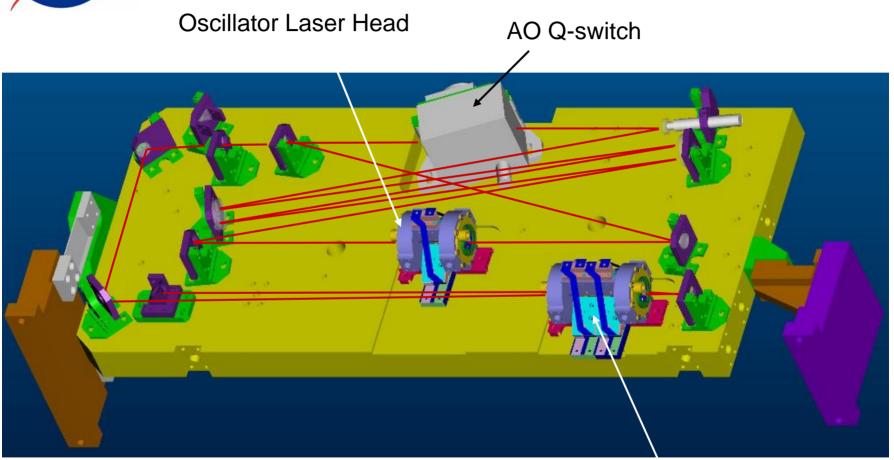
- Modular approach with injection seed & local oscillator separate from transceiver.
- Separate seed/LO allows flexibility to adapt to 4 measurements scenarios:
  - -simple, fixed frequency LO for ground or low platform speed.
  - higher intermediate frequency for high platform speed
  - swept LO for very high platform speed.
  - -DIAL of  $CO_2$



Note: only optical paths are represented; electrical and water paths are not shown.



### LRRP Pulsed, 2-Micron Laser Transmitter Opto-Mechanical Design



• 3-m, bow-tie, unidirectional master oscillator power amplifier

• Seeding and receiver optics on reverse side

Expect this hardware in about 8 weeks for LRRP

**Amplifier Laser Head** 



## Seed Laser



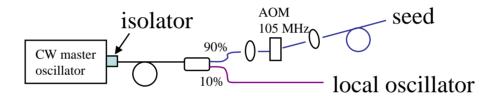


CW seed laser

Seed laser driver



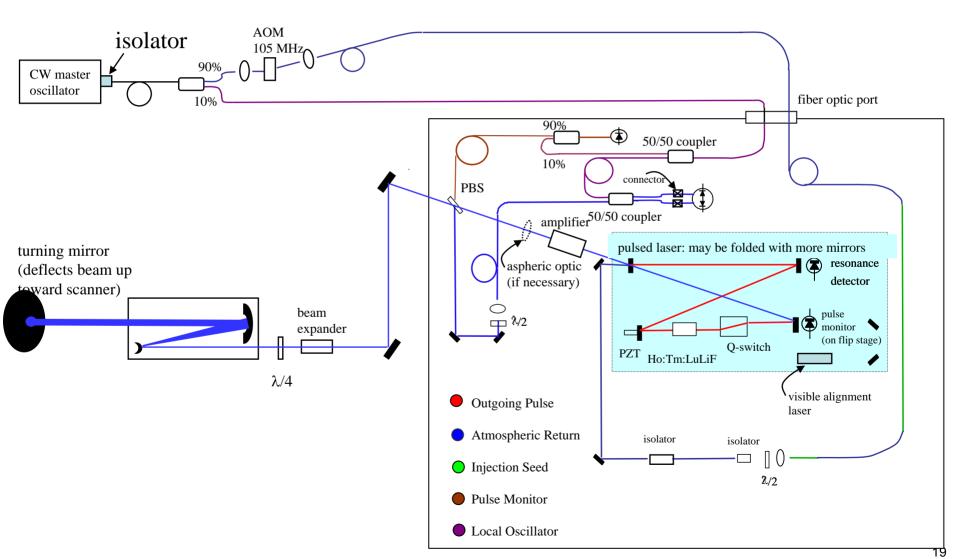
# Seed/LO Option 1



- baseline design for ground-based implementation.
- recommended for IIP demonstration.
- fiber-to-free space through AOM then back to fiber is disadvantageous—looking into fiber optic pigtailed AOM.
- could be packaged in rack-mount breadboard with fan for cooling (need thermal analysis).

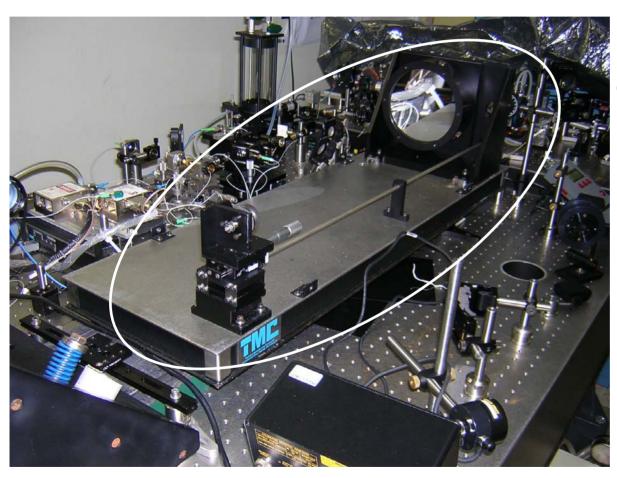


## Test Bed: Putting it all Together





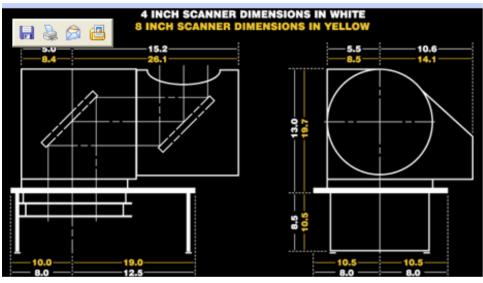
# VALIDAR Telescope



- off axis Dall-Kirkham design.
- 6-inch aperture
- 20X expansion



### VALIDAR Scanner



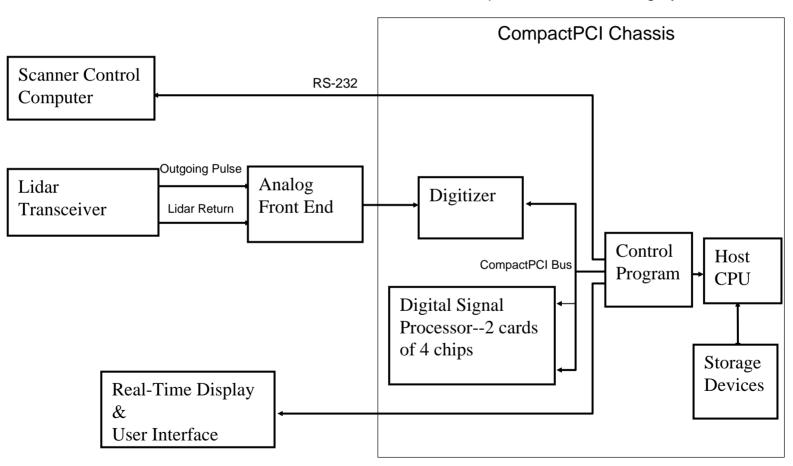
- scanner is mounted on roof of laboratory trailer.
- 8-inch clear aperture.
- can be pointed or scanned in elevation/azimuth for hemispherical coverage.
- linked to data acquisition computer for automated profiling of wind.





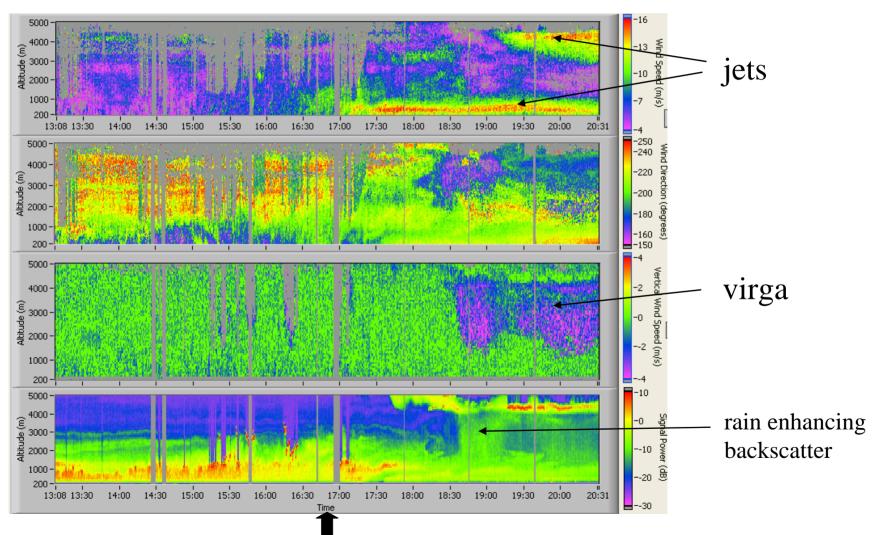
### Data Acquisition and Processing (already built)

#### Data Acquisition and Processing System





# Atmospheric Measurements (will be better than this VALIDAR sample)





# Summary

- IIP project 6 months into 36 month effort
- On schedule and budget to date
- Leveraging LRRP work on compact laser in 05 and 06
- Plan on significant steps of compact, engineered packaging of stateof-the-art laser/lidar technology. TRL definitions do not reveal significant progress.
- Companion IIP at GSFC for noncoherent Doppler wind lidar will complement this project to permit hybrid DWL on aircraft and then in space
- Project very consistent with findings of NASA/ESTO Laser/Lidar Technology Requirements Working Group results (FY06). To be issued in final report
- Anticipate strong endorsement of global winds by NAS decadal study on earth sciences
- Same technology promises additional applications for earth and Mars



# Project Motto 1

Be Prepared





# Project Motto 2





# **BACK UP**



## IIP – Scope of the Project



### Pulsed Doppler Wind Lidar Measurement Scenario

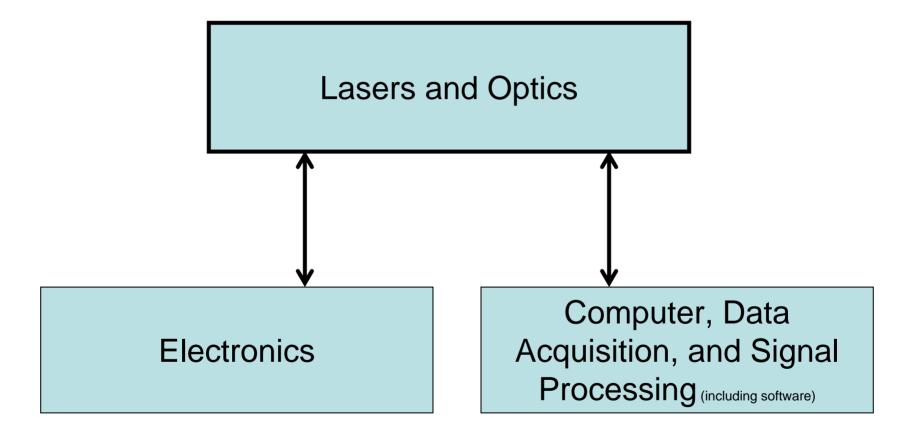
Target (Atmospheric Aerosols)

Propagation Path (Atmosphere)

Lidar System

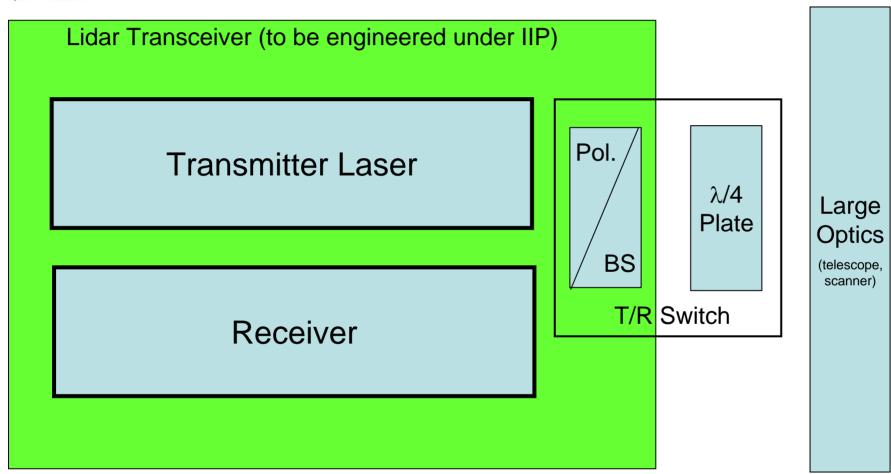


### Lidar System



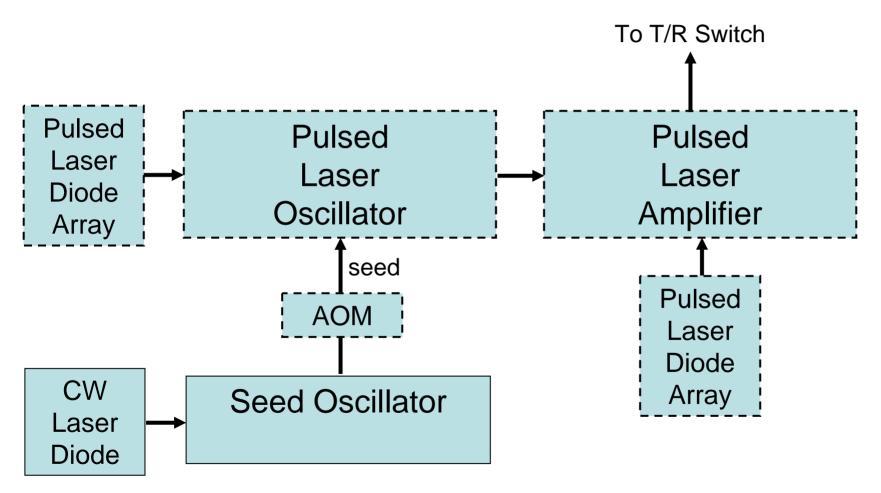


### Lasers and Optics



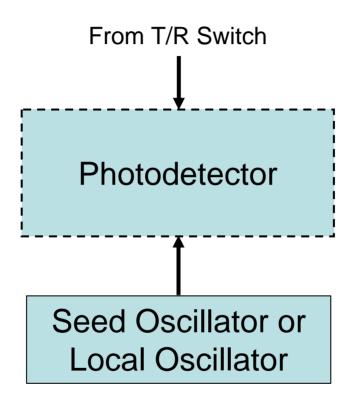


### **Transmitter Laser**





### Receiver







# Laser Design Considerations

- Laser wavelength
- Laser material
- Laser pumping geometry
- Laser cavity design
- Laser architecture



# Why Ho:Tm:LuLiF

### • Why Ho laser?

- Tm lasers in 2-μm region have such a low gain cross-section  $(\sigma_{em} \sim 10^{-20} \text{ cm}^2)$  that efficient, high-energy laser amplification is impossible without the risk of laser crystal or associated optics damage.
- Ho lasers have large enough stimulated emission cross-section  $(\sigma_{em} \sim 10^{-19} \text{ cm}^2)$  for effective amplification to obtain high-energy.

### Why co-doped?

- Takes advantage of diode pumping for Tm lasers
- Takes advantage of the efficient Tm 1:2 relaxation energy transfer process
- Takes advantage of the high emission cross-section of Ho laser



# Why Ho:Tm:LuLiF — Cont.

- Why fluoride?
  - Fluoride
    - Long upper laser level lifetime ~ 15 ms, store more energy
    - Low up-conversion loss
    - Higher emission cross-section
    - Naturally birefringent material, no depolarization loss
    - Negative dn/dT -> weak thermal lensing
  - Garnet
    - Isotropic
    - Excellent thermo-mechanical properties
- Why Lutetium?
  - Lanthanide series ions
    - Lutetium, Yttrium, Gadolinium
  - Lutetium
    - Lutetium larger crystal field
      - larger manifold stark splitting -> Small thermal population of ground state



### Laser Architecture

### Master Oscillator Power Amplifier (MOPA)

- Energy requirement
  - Single oscillator can't produce required energy
- Beam quality
  - MOPA preserves the good beam quality
- Lifetime
  - Permits more derating of pump diodes
- Efficiency
  - Multiple pass amplifier improving the efficiency
- Optics Damage
  - Reducing intra-cavity fluence



## **Cavity Configuration**

- Linear Cavity
  - Standing waves
  - Simple
  - Round trip pass gain medium twice
- Ring Cavity
  - Traveling waves
  - No spatial hole burning in the gain-> single mode
  - Long cavity needed to obtain narrow linewidth
  - Beneficial for injection seeding through output coupler



## Pumping configuration

- Pumping geometry
  - Side Pumping
    - » Power scaling
    - » Uniform pumping
  - End Pumping
    - » Easy thermal management
    - » Easy to mode match
    - » Higher pump density
- Single Longitudinal Mode
  - Interferometric mode selection
  - Monolithic design, short cavity
  - Injection seeding



# **Optical Bench**

Two options:

26.5 x 23.0 x 7 inch single side

26.5 x 11.5 x 7 inch double sided

- The split can be done such that the receiver optics and the seed laser on one side, and the power Oscillator amplifier on the other.
- Optical bench is water cooled, enclosed and dry purged.